



Wellington Central Library, 101 Wakefield Street, Wellington

Targeted Damage Evaluation Report following the November 2016 Kaikoura Earthquakes

**Wellington City Council** 

15 February 2017 Revision: 0

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## Document control record

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## 1 Executive Summary

This assessment has been carried out at the request of Aurecon's client, Wellington City Council for the Wellington Central Library at 101 Wakefield Street, Wellington.

The fundamental objective of a Targeted Damage Evaluation (TDE) requested by the Wellington City Council (WCC) is to identify and review the primary vertical and lateral load paths of specific buildings that fall under the Affected Building Profile and carry out an assessment of the damage to critical areas of the structure.

The document, Engineering Guidelines for Targeted Damage Evaluation following the November 2016 Kaikoura Earthquakes, Version 1.1 – 25 January 2017 produced by the Society of Structural Engineers (SESOC), New Zealand Society for Earthquake Engineering (NZSEE) and WCC has been used as the basis of this investigation.

In this assessment, Aurecon structural engineers carried out intrusive investigations in specific locations to determine the extent of damage to the building. Cladding and lining materials were removed to expose the primary structure in various 'hot-spot' locations identified in a desktop study of the available documentation. The damage to the structure is discussed in Section 5.

From the 2016 Kaikoura earthquake the majority of the structure suffered only minor damage. Existing damage was observed in particular at the precast units of the ground floor level most of which have had support sections retrofitted in order to rectify any risk of failure in 2013.

The only area of concern identified in the inspections was a single precast floor unit at ground floor which was found to have a crack which could compromise its capacity (CDS A). This damage appears to be recent as no additional support has been installed to this unit, but it is typical when compared to previous damage to adjacent units which have had remedial works applied.

No evidence of plastic hinge formation was observed in seismic beams and columns, no beam elongation was observed and no loss of seating of the hollowcore floor units was seen. Several cracks were observed in the levelling compound floor topping in the proximity of the perimeter columns. Further investigations showed the cracks to be only superficial. The crack sizes were less than 0.5mm wide on the levelling compound.

Aside from the localised floor area mentioned above, it appears that the damage observed will not affect to the performance of the building or pose a risk in future earthquakes or aftershocks and it is therefore not necessary to change the current occupancy. The exterior cladding panels appear to be adequately fixed to the structure and do not pose a life safety hazard to occupants, passing pedestrians or neighbouring buildings. Furthermore, the internal egress paths including stairs do not appear to have any damage that would limit their performance or cause failure resulting in egress routes being blocked.

## 2 Description of Structure

As identified by the WCC, the Wellington City Library falls under the category of 'Affected Building Profile' due to a combination of its structural form, size and siting.

The building was designed and documented in 1989 in accordance with loading standards NZS4203:1984 and the concrete structures standard NZS3101:1982. The building is a six storey reinforced concrete frame structure constructed on flat ground. The building consists of a basement level, full height mezzanine level, three levels of library space and 2 levels for office use.

The structural system of the building consists of reinforced concrete moment resisting frames in the longitudinal and transverse directions with perimeter walls at basement level. The typical flooring system consists of precast pre-stressed hollowcore units with an in-situ topping spanning in the longitudinal direction of the building. Cladding to the structure includes precast concrete panels with window penetrations on three sides of the building, the remaining façade of the building has a glazed curtain wall system. The building foundations are made up of a series of bored reinforced concrete piles. Biaxial actions on "corner" columns has been limited by creating pin-end beam connections in one of the frame joining into these columns.

The concrete piles are generally belled at the base and are approximately 5-6m in length below the basement floor slab. The piles have been founded in dense gravels that underlie the site. The site is classified as 'Type C' subsoil in accordance with NZS 1170.5

Previous repair work to the building was observed at the basement level. Steel brackets have been installed to support hollowcore units due to transverse cracking. This repair work was designed by Holmes Consulting Group and installed in 2013/2014.

Figure 1 and 2 below show two views of the building, western elevation from Victoria Street and the eastern elevation from Civic Square. A typical floor plan of the building is shown in Figure 3.







Figure 2 - View of the Wellington City Library from Civic Square

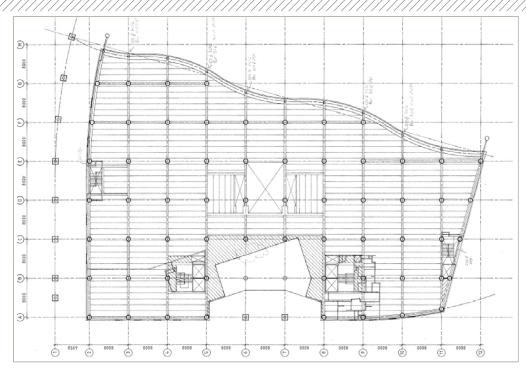


Figure 3 – First Floor Plan

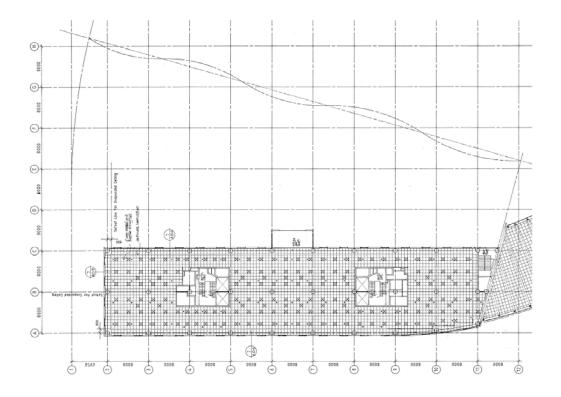


Figure 4 – Fourth Floor Plan

## 3 Inspections and Assessments Undertaken

### 3.1 Dates and Scope of Inspections and Assessments

Following the November 2016 earthquakes, Rapid Assessment investigations were carried out by Aurecon engineers Adonia La Camera and Mehrdad Seifi on 14 November 2016. The Rapid Assessment Form is attached in Appendix A.

The TDE inspections were carried out in accordance with the procedures documented in the SESOC guidelines. Structural engineers from Aurecon, Adonia La Camera and Jagnesh Makwana, carried out inspections in January and February 2017.

The scope of these inspections was to investigate the extent of damage to the building and in particular focus on damage to specific areas as follows:

- Cracking to hollowcore units for all levels
- Elongation of frames and seating damage leading to loss of support for precast flooring systems
- Disconnection of gravity load system for diaphragms, particularly in frames running parallel to the floor span
- Damage to beams and columns
- Identification of critical damage to stairs
- Identification of critical damage to support points of heavy cladding systems

#### 3.2 Intrusive Investigations

As part of this evaluation the carpet was rolled back in several locations to reveal the top of the floor slab and ceiling tiles were lifted to expose the underside of the floor slab. In a few locations on each floor 10mm from the top of the concrete slab was removed to check if surface cracks were penetrating deeper into the slab.

Plaster surrounding a column that was cracked was removed to investigate the integrity of the column. 10mm of cover concrete was removed from a beam to investigate if cracking observed was superficial or structural. Furthermore, some of the beam column joint cover concrete was removed to check the integrity of the beam to column pin end connection.

Wall linings and concrete topping were removed to expose the bottom connection of the precast panels.

#### 3.3 Building Inspections

The initial inspection was carried out on the 27<sup>th</sup> of January 2017. Subsequent inspections were carried out on the 3<sup>rd</sup>, 7<sup>th</sup>, 9<sup>th</sup>, and 10<sup>th</sup> of February 2017.

#### 3.4 Pre-Earthquake Seismic Assessments

A seismic assessment was undertaken by Holmes Consulting Group in 2013 which determined the building to have a global seismic rating of 60% NBS (New Buildings Standard). However the stairs were rated between 35-45% NBS. The precast panel connection scored 40% NBS and the precast hollowcore unit seating was between 35-45% NBS.

## 4 Information Sources

### 4.1 Available Documentation

Full structural and architectural drawings were available provided by the WCC Archives and the original building designers, Holmes Consulting Group and Athfield Architects. Only partial mechanical and electrical service documentation was retrieved from the WCC Archives.

## 5 Damage Observed

#### 5.1 Overview of Damage Observed

The damage noted to the primary structure consisting of reinforced concrete moment resisting frames were minor or insignificant.

Damaged observed during the intrusive investigation is summarised below. Reference should be made to Appendix C for photographs of damage to specific areas of the building with comments.

- No evidence of plastic hinge formation in the seismic beams and columns observed. Hairline cracks were noted in the potential plastic hinge zones of beams in several locations but no spalling or growth in the length of the beams was observed. Spalling of concrete cover was observed at the bottom of the pin-end beam/column connections which are expected and do not downgrade the system capacity. No damage was observed to columns. In Appendix C see photos 18, 22, 23, 26.
- No separation of the floor slab from the perimeter frames was observed where precast hollowcore units run parallel to the perimeter beams.
- No loss of seating to the hollowcore units was noted at support beam locations. There was minor spalling showing signs of movement in a few locations but no loss of seating was observed.

Several cracks were noted in the levelling compound floor topping on several floor levels, in particular at the proximity of columns on the perimeter of the building. Several cracks propagate from the face of the columns are short and decrease in width. The width of the cracks were less than 0.5mm. In certain locations the floor levelling compound and 10mm of concrete topping was removed to check the vertical extension of the crack which was generally found to terminate within this 10mm depth. In one case the vertical crack penetrated through the entire slab depth. This was in the location where steel support brackets were provided following the earthquake in 2013.

No signs or damage or cracking was observed to the underside of hollowcore units above the ground floor. Several cracks were observed at the ground floor level. The majority of these cracks were already identified by investigations done by Holmes Consulting Group in 2013 and additional support brackets installed.

Only one crack is found on a single hollowcore precast unit to be of concern and classified as CDS A in accordance with the TDE Guidelines which will require repair work. This is a transverse crack across a hollowcore unit on ground level Grid 9/B-C. The dimension of the panel is 8m x 1.2m. Figure 5 shows the location.

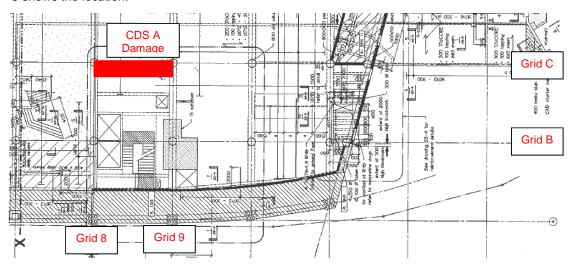


Figure 5 – Location of transverse crack to hollowcore ground floor unit



Figure 6 – Transverse crack to hollowcore ground floor unit. CDS A damage.

Refer Appendix C for photos (No. 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 13, 14, 15, 16, 27, 28, 29, 30, 31) related to floor cracking.

- No structural damage was observed to the steel structure supporting the central stairs. In particular the connection of the stair landing to concrete beam showed no signs of movement or cracking. The precast concrete emergency stairs suffered only minor damage at the landing joint connection which does not compromise the safety of the stairs. The external stairs running from Civic Square had damage to tiles due to an insufficient gap between the external stairs and the building. Damaged tiles were replaced soon after the earthquake. Refer Appendix C photos (No. 24, 25) related to stairs investigations.
- No signs of damage or inadequate movement was observed for the precast cladding panels and their connections. Refer Appendix C for photos (No. 12, 13, 19, 20, 21) related to cladding panels.

Other damage noted to the structure thought to be unrelated to the 2016 Kaikoura earthquake include:

- Small cracks to the blockwork walls noted in the basement of the building which are not a concern.
- Shrinkage cracks (~0.1-0.5mm wide) seen in the concrete topping of the carpark floors.

## 6 Assessment

Based on the extent and nature of the damage observed, we believe there is no need for the occupancy of the building to be changed. However, the area above and below the damaged hollowcore unit needs to be vacant until propping has been provided. Repair works are required to restore the integrity of the floor unit in one location.

## 7 Further Actions Proposed

No further investigations are required.

# Appendix A Rapid Assessment Forms



# EARTHQUAKE RAPID ASSESSMENT FORM

## Complex Residential and all Non-Residential Buildings Level 2

			Married Charles and Charles	CONTRACTOR OF THE PROPERTY OF			
ASSESSMENT			Fields with asterisks (*) an	mandatory, others are optional.			
1 Assessor Name*	EHRDAD	SEIFIA	DONIA CA	9 MERA			
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2 Assessment Date*	Day Month Year	Assessment Time*	Hour Minute to nearest half hour)	AM B PM			
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Unit / Number*							
Street*	ICTORIA	ST.					
City/Town*	EIII INGT	ON					
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GPS (Degree with 5 decim	ais after comma) South		ken A○No B○Yes F	Photo ID			
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	Owner B  Ten	ant c Other	Property Manage	er.			
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Phone (with area code)	1						
5 Existing Placard* 1	<b>○ Y</b> 2	Jare	Day Month Year	m ID*			
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				Cladding Tupo			
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Storeys above ground	A <1935 B 1935-1976	A Complex residential  B School	A Timber frame  B Steel frame	A Brick veneer  B Concrete panels			
Storeys above ground incl. ground floor	A <1935 B 1935-1976 C 1977-1984	A Complex residential  B School  C Commercial/Office	A Timber frame  B Steel frame  C Concrete frame	A Brick veneer			
Storeys above ground incl. ground floor  Storeys below ground	A <1935 B 1935-1976 C 1977-1984 D 1985-2000	A Complex residential  B School	A Timber frame  B Steel frame	A Brick veneer  B Concrete panels  C Steel			
Storeys above ground incl. ground floor  Storeys below ground	A <1935 B 1935-1976 C 1977-1984 D 1985-2000	A Complex residential  B School  C Commercial/Office  D Industrial	A Timber frame  B Steel frame  C Concrete frame  D Concrete shear wall	A Brick veneer  B Concrete panels  C Steel  D Glass			
Storeys above ground incl. ground floor  Storeys below ground  Footprint (m²)	A <1935 B 1935-1976 C 1977-1984 D 1985-2000 E >2000	A Complex residential  B School  C Commercial/Office  D Industrial  E Critical facility	A Timber frame  B Steel frame  C Concrete frame  D Concrete shear wall  E Tilt-up concrete	A Brick veneer  B Concrete panels  C Steel  D Glass  E Lightweight			
Storeys above ground incl. ground floor    5	A <1935 B 1935-1976 C 1977-1984 D 1985-2000 E >2000	A Complex residential  B School  C Commercial/Office  D Industrial  E Critical facility  F Public assembly	A Timber frame B Steel frame C Concrete frame D Concrete shear wall E Tilt-up concrete F Reinforced masonry	A Brick veneer  B Concrete panels  C Steel  D Glass  E Lightweight			
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	Damag							Damage				
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Overall Hazard*	N/A	А	В	С	D	Non-structur	al Hazards*	N/A	А	В	С	D
1 Collapse or partial collapse	Ø	0	0	0	0	11 Parapets, orna chimneys	amentation,	0	0	0	0	0
2 Building or storey leaning	0	0	0	0	0	12 Cladding, glaz	ing	0		Ø	0	0
3 Other:	0	0	0	0	0	13 Ceilings, light	fixtures	0	0	0	<b>3</b>	0
Structural Hazards*	N/A	А	В	С	D	14 Interior walls,	partitions	0	0	<u> </u>	8	0
4 Foundations	0	0	0	0	0	15 Access/egress (elevators, star		0	0	0	0	0
5 Roofs, floors	0	0	0	Q	0	16 Significant fire concerns		0	0	0	0	0
6 Gravity systems (columns, beams, etc)	0	0	0	D	0	17 Utilities (e.g. g waste water, p	as, electricity,	0	6	0	0	0
7 Lateral systems (walls, frames, braces)	0	0	0	0	0	18 Other:		0	0	0	0	0
8 Diaphragms, horizontal bracing	0	0	0	0	0		Stairs					_ <u>_</u>
9 Precast connections	0	0	0	0	0	Comments:	0,4,0					
10 Other:	0	0	0	0	0							
Recommended furthe	er Assessment* Safety Cordon* Barricades* Urgency of suggested ac					ction*						
A None B Level 2 Rapid Assessment (tick below if particular expertise is required) B1 Structural Engineer B2 Geotechnical Engineer B3 Other:			Describe extent (add diagram on separate sheet if required)  C Barricades  Describe extent ( separate sheet if		s already in place s required (add diagram on		A Standard  B Immediate action required					
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**⊘**No

Sketch included on separate page? Yes

VERSION 01 - APRIL 2014

# Appendix B Standardised Summary Table

Standardised Summary Table: Targeted Damage Evaluation Data V1.23 All RED cells must be filled in prior to submission. Location Building Name: Bldg D - Wellington Central Library Assessing Engineer Adonia La Camera No: Street CPEng No Building Address: Compan Aurecon NZ Ltd Legal Description: Lot 1 DP 494594 CFR 724107 Company project number 254449 Company phone number 04 472 9589 GPS south: Date of submission Inspection Date Revision Building Unique Identifier (WCC BUFI number): Is there a full report with this summary? Available documentation Architectural full original designer name/date original designer name/date Athfield Architects Ltd / 1990 Structural Holmes Consulting Group / 1990 original designer name/date original designer name/date Mechanical partial Rankine & Hill Limited / 199 Electrical partial Rankine & Hill Limited / 1990 Geotech report none original designer name/date NA Site Surrounding Site slope: flat 3.5 Flat Soil type: Other fill
Site Class (to NZS1170.5): C Soil Profile (if available): No 4.00 In reclamation zone? If Ground improvement on site, describe Proximity to ocean (m, if <100m): Approx site elevation (m): Building Ground floor elevation (Absolute) (m): 4.00 No. of storeys above ground (excl. mezzanine): single storey = 1Mezzanine? yes Ground floor split? no Ground floor elevation above ground (m): 0.00 Storeys below ground Foundation type: bored Building height (m): 23.00 if Foundation type is other, describe: Floor footprint area (approx): 3360
Year of construction: 1990 Year of design: Is the building consistent with the Structural drawings? yes If no describe variation in report If so, when (year)? And what load level? Seismic Strengthening/retrofit present? Use/occupancy (ground floor): Use/occupancy (upper floors): Type of strengthening/retrofit Securing of non-structural elements Use/occupancy notes (if required): Library and office use Importance level (to NZS1170.5): IL2 First storey height (m) Plan irregularity: significant 6.80 Vertical irregularity severe Typical storey height (m) 4.50 Other irregularity Gravity Structure Gravity System: Roof system: concrete
Beams: precast concrete slab thickness (mm 65 overall depth (mm 865 900 diamete Columns: cast-insitu concrete typical dimensions (mm x mm Walls: partially filled concrete masonry Floor Diaphragm: Type of floor system Topping thickness (slab if CIP) (mm) [describe using options below] Topping (slab if CIP) reinforcement Precast unit type describe if hollowcore units are spaced with timber infill Precast unit depth (mm) Precast unit seating deta Low friction bearing strip used Beam to slab continuity reinforcement Link slab between precast units and frame If yes, describe link slab (including width and thickness) # bays of frames spanning parallel to single precast unit Ties from columns into floor (for least restrained column diagonal or straight column ties? Straight column ties Lateral system along: Note: Define along and across note typical bay length (m) Closest direction to "along": NE-SW in detailed report! Design Ductility assumed, μ: 3.00 Period along: 1.83 estimate or calculation? calculated Total deflection (ULS) (mm): 457 maximum interstorey deflection (ULS) (mm): 130 estimate or calculation? estimate or calculation? calculated Lateral system across: note typical bay length (m) Closest direction to "across": NW-SE Design Ductility assumed, µ: 3.00 Period across: 1.45 calculated Total deflection (ULS) (mm): 411 estimate or calculation? calculate maximum interstorey deflection (ULS) (mm): 120 estimate or calculation? calculated Separation from neighbouring structures: north (mm): leave blank if not relevant east (mm) south (mm) west (mm): Non-structural elements (fill in matrix) Damaged in EQ? Threat to Life Safety? Threat to Egress? Stairs: Wall cladding: precast panels
Roof Cladding: Other (specify) no no no Glazing: aluminium frames no no no no Sprinkler system with localised manual cal Fire suppressant system: points, smoke detectors and sounders VAV system to office floors generally, CV unknown unknown unknown system to main public library area, with supplementary FCUs to perimeter glazing Heating and Ventilation system: areas of office floors Elevator: yes
Other heavy or hazardous elements: Machinery no \*reference Targeted Damage Evaluation Guidelines for description of each damage type Critical Damage States Evaluation for RC Buildings\* Damage posing collapse risk (A and B) Where multiple cases observed, fill in for worst case Transverse crack at end of hollowcore (top of slab): Max crack width If cracked, how many units with damage Web cracking? Closest crack distance to beam support (mm) Vertical offset at crack? Transverse crack at end of hollowcore (bottom of unit): Max crack width If cracked, how many units with damage Closest crack distance to beam support (mm): Vertical offset at crack? Transverse crack at end of ribs If cracked, how many units with damage: Max crack width

Closest crack distance to beam support (mm):

Estimated seating lost due to damage (mm): Estimated seating lost due to beam elongation (mm):

If damaged, how many units with damage:

Inclination of crack

Vertical offset at crack?:

Damage to support of precast unit:

Remaining precast unit support: Evidence of beam elongation:

Loss of column lateral support: insignificant	Note: Mesh does not count as ties	How many columns affected?	
Shear cracks in columns: none		How many columns affected?	
mage posing lower risk (C)			
Column Plastic Hinge damage - Criterion 1 met? no damage	Hinge damage criteria:	Describe damage as per criterion 1	
Criterion 2 met? no damage		Describe damage as per criterion 2	
Criterion 3 met? no damage	1. Total crack width in plastic hinge >	Describe damage as per criterion 3	
Criterion 4 met? no damage	0.005d	Describe damage as per criterion 4	
Location of critical column plastic hinge: NA	2. Sliding has occurred on a crack		
Beam Plastic Hinge damage - Criterion 1 met? no damage	2. Shamig has occurred on a crack	Describe damage as per criterion 1	
Criterion 2 met? no damage	3. Wide (>0.5mm) diagonal cracks	Describe damage as per criterion 2	
Criterion 3 met?	4. Concrete degradation, indicated	Describe damage as per criterion 3	
Criterion 4 met? damage but criteria not met	Concrete degradation, indicated by significant spalling (concrete cover can be removed by hand)	Describe damage as per criterion 4 Occurred at the pinned	beam locations
Location of critical beam plastic hinge: NA			
Wall Plastic Hinge damage - Criterion 1 met? no damage		Describe damage as per criterion 1	
Criterion 2 met? <mark>no damage</mark>		Describe damage as per criterion 2	
Criterion 3 met? no damage		Describe damage as per criterion 3	
Criterion 4 met? no damage		Describe damage as per criterion 4	
Location of critical wall plastic hinge: NA			
Web cracking of Hollowcore none known		If cracked, how many units with damage:	
Longitudinal cracking of hollowcore fully developed, with reinf in topping in	ntact	If cracked, how many units with damage: 3	
Mesh fracture none observed			
mage to other elements posing life-safety risk			
Stairs no significant damage		Describe damage: Minor damage at the lar	nding joints
Heavy cladding no significant damage		Describe damage:	
Heavy overhead non-structural elements not applicable		Describe damage:	
uilding Closure			
Was the building closed following the earthquake? yes  If yes, from when 14/11/2016	dd/mm/yyyy		
If yes, to when 17/11/2016	dd/mm/yyyy		
If yes, what was the reason(s)  Non-structural damage (including inte			
(use all that apply, in priority order)  L1/L2 assessments	Small algreatest phoney		
(if "other", please specify in notes)			
( ) ( )			
commendations			
		Repair Hollow core pane	el at Ground Floor
Repair/strengthening recommended: significant structural		Describe: Level	
Building Consent required: unknown		Describe:	
		V	domonod H-II-II
Interior acquirency recommendations. Continued		Vacate the area above	
Interim occupancy recommendations: Continued normal occupancy		Describe: core panel until proppino	y is been provided
External barricading of public spaces recommended? no		Describe:	
icial Use only:			
Accepted By		Initial WCC review by:	
Date:	F	urther review by (or indicate Not Required):	

# Appendix C Photographs of Damage

ID.	Location & comments	Photographs
1.	Underside of Ground Floor Level Grid 3/B-C.  Diagonal crack. This crack was existing as observed from a photo taken in 2013.	
2.	Underside of Ground Floor Level Grid 5/B-C.  Longitudinal cracking in the direction of floor span. This crack was existing as observed from a photo taken in 2013.	
3.	Underside of Ground Floor Level Grid 6/C. Transverse cracking (perpendicular to the direction of floor span). Occurred following the earthquakes in 2013. Support brackets provided.	

4. Underside of Ground Floor Level Grid 9/B-C.
Significant transverse cracking (perpendicular to the direction of floor span). Its width range between 1 and 2 mm. The panel needs to be repaired.



5. Underside of Ground Floor Level Grid 9/B-C.
Significant transverse cracking (perpendicular to the direction of floor span). Its width range between 1 and 2 mm. The panel needs to be repaired.



6. Underside of Ground Floor Level Grid 9/B-C.
Significant transverse cracking (perpendicular to the direction of floor span). Its width range between 1 and 2 mm. The panel needs to be repaired.



7. Underside of Ground Floor Level Grid 7/A-B.
Transverse cracking (perpendicular to the direction of floor span). This crack was existing as observed from a photo taken in 2013.



8. Underside of Ground Floor Level Grid 8/F.

Transverse cracking

Transverse cracking (perpendicular to the direction of floor span). This crack was existing as observed from a photo taken in 2013.



9. Underside of Ground Floor Level Grid 6/B.

Diagonal cracking (perpendicular to the direction of floor span) adjacent to column. This crack was existing as observed from a photo taken in 2013.



Ground Floor cracking adjacent to column near Grid 11/A.

Crack width on the levelling compound less than 0.5mm.



11. Second Floor cracking adjacent to column near Grid 11/A.

Further investigations showed the crack to be only superficial.



12. First Floor cracking adjacent to column on Grid 12/E.

Those cracks behind the beams are not structural. They define the area above the bottom precast cladding connections.



13. Ground Floor cracking adjacent to column on Grid 2/B. 14. No signs of cracking on Ground Floor adjacent to column on Grid 2/G No signs of 15. cracking on Ground Floor adjacent to column on Grid 4/E

16. Second floor cracking adjacent to column on Grid 10/D.



17. Fourth floor cracking on perimeter of building adjacent to precast panels Grid 2/C. Those cracks behind the beams are not structural. They define the area above the bottom precast cladding connections.



18. No signs of cracking to column on Grid 4/A on mezzanine level.





19. No signs of earthquake damage to precast panels connections on fourth level Grid 2-3/C.



20. No signs of earthquake damage to precast panels connections on third level Grid 10-11/A.





21. Extrusive investigation of third level slab at precast panel junction on Grid 11/A indicating no significant signs of earthquake damage.



22. Minor spalling to mezzanine level reinforced concrete beam on Grid 4/A.



23. No signs of recent earthquake damage to mezzanine level reinforced concrete beam on Grid 5/A.



24. No significant signs of earthquake damage to stair landing between third and fourth floor levels in south core stairwell.





25. Gap opening of joint between stair units in Harris Street end stairwell.



26. No notable earthquake damage to ground floor columns and beams.





27. Superficial crack to ground floor on Grid 4/E-F



28. Cracking to ground floor on Grid 6/F-G



29. Ground floor cracking near Grid 9/F.

Crack width ~1.0mm.
Steel bracket supports are provided below this crack following the 2013 earthquake.



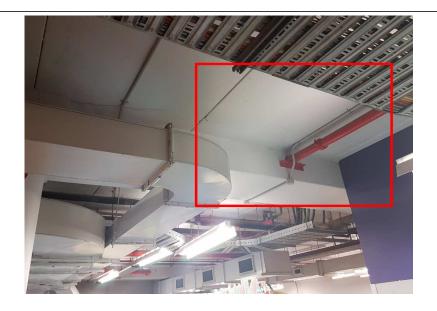
30. Ground floor cracking on the top of the slab near Grid 9-10/B.

Crack width ~0.6mm.



31. Ground floor panels near Grid 9-10/B.

No crack observed in the area inside the red square.





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